

APPENDIX II.

TABLE CIX.—SHOWING RELATION OF PERCENTAGE OF CARBON TO TENSILE STRESS.

It is extremely difficult to give the tensile stress corresponding to different percentages of Carbon in commercial steels, as the strength of the material for the same Carbon content will vary according to the process of manufacture, the size of the finished section, and the percentages of other impurities present. The following table gives, approximately, what may be expected from steel of good quality in which the Manganese does not exceed .8 per cent. When Manganese is above .8, the tensile stress will be considerably higher. The table has been compiled from a large number of published results, and from the author's private records. The tensile stress for basic steels above .5 is not given, as so little high Carbon basic steel is made in this country that a sufficient number of samples have not been available to obtain a fair average.

Acid Bessemer and basic Bessemer steels will not differ greatly from open hearth steel in tensile strength, especially in the low Carbon steels, and comparatively little high Carbon steel is made by these processes, except for rails.

ACID OPEN HEARTH STEEL.			BASIC OPEN HEARTH STEEL.		
Carbon per cent.	Tensile Stress.		Carbon per cent.	Tensile Stress.	
	Tons per Square Inch.	Lbs. per Square Inch.		Tons per Square Inch.	Lbs. per Square Inch.
.05 to .10	21 to 27	47,040 to 60,480	.05 to .10	20 to 25	44,800 to 56,000
.10 " .15	24 " 29	53,760 " 64,960	.10 " .15	23 " 27	51,520 " 60,480
.15 " .20	27 " 32	60,480 " 71,680	.15 " .20	25 " 29	56,000 " 64,960
.20 " .25	29 " 34	64,960 " 76,160	.20 " .25	26 " 30	58,240 " 67,200
.25 " .30	30 " 35	67,200 " 78,400	.25 " .30	28 " 32	62,720 " 71,680
.30 " .35	31 " 37	69,440 " 82,880	.30 " .35	29 " 33	64,960 " 73,920
.35 " .40	35 " 41	78,400 " 91,840	.35 " .40	31 " 35	69,440 " 78,400
.40 " .45	39 " 45	87,360 " 100,800	.40 " .45	34 " 40	76,160 " 89,600
.45 " .50	43 " 48	96,320 " 107,520	.45 " .50	38 " 43	85,120 " 96,320
.50 " .55	47 " 53	105,280 " 118,920			
.55 " .60	50 " 55	112,000 " 123,200			
.60 " .65	52 " 57	116,480 " 127,680			
.65 " .70	55 " 60	123,200 " 134,400			
.70 " .75	58 " 62	129,920 " 138,880			
.75 " .80	60 " 64	134,400 " 143,360			
.80 " .85	61 " 65	136,640 " 145,600			
.85 " .90	63 " 67	141,120 " 150,800			

NOTE TO TABLE C. (pp. 517-521).

To obtain the relation of stresses over 50 tons on the square inch, multiply or add two of the lines of figures given in the table. For instance, to find the number of kilos. per square mm. answering to 60 or 65 tons on the square inch:—

Multiplication.

$$\begin{array}{r} 30 \text{ tons per square inch} = 47.25 \text{ kilos. per square millimetre.} \\ 2 \\ \hline 60 \text{ " " " " } = 94.50 \text{ " " " " } \end{array}$$

Addition.

$$\begin{array}{r} 50 \text{ tons per square inch} = 78.75 \text{ kilos. per square millimetre.} \\ 15 \text{ " " " " } = 23.62 \text{ " " " " } \\ \hline 65 \text{ " " " " } = 102.37 \text{ " " " " } \end{array}$$

APPENDIX III.

TABLE CX.—SHOWING HOW TONS PER SQUARE INCH AND LBS. PER SQUARE INCH COMPARE WITH KILOGRAMMES PER SQUARE MILLIMETRE.

(Calculated by JOHN W. HALL.)

Tons per Sq. In.	Lbs. per Sq. In.	Kilos. per Sq. Mm.	Tons per Sq. In.	Lbs. per Sq. In.	Kilos. per Sq. Mm.	Tons per Sq. In.	Lbs. per Sq. In.	Kilos. per Sq. Mm.
10.00	22,400	15.75	12.55	28,112	19.77	15.05	33,712	23.70
10.05	22,512	15.83	12.60	28,224	19.84	15.10	33,824	23.78
10.10	22,624	15.91	12.65	28,336	19.92	15.15	33,936	23.86
10.15	22,736	15.99	12.70	28,448	20.00	15.20	34,048	23.94
10.20	22,848	16.06	12.75	28,560	20.08	15.25	34,160	24.02
10.25	22,960	16.14	12.80	28,672	20.16	15.30	34,272	24.10
10.30	23,072	16.22	12.85	28,784	20.24	15.35	34,384	24.18
10.35	23,184	16.30	12.90	28,896	20.32	15.40	34,496	24.25
10.40	23,296	16.38	12.95	29,008	20.40	15.45	34,608	24.33
10.45	23,408	16.46				15.50	34,720	24.41
10.50	23,520	16.54	13.00	29,120	20.47	15.55	34,832	24.49
10.55	23,632	16.62	13.05	29,232	20.55	15.60	34,944	24.57
10.60	23,744	16.69	13.10	29,344	20.63	15.65	35,056	24.65
10.65	23,856	16.77	13.15	29,456	20.71	15.70	35,168	24.73
10.70	23,968	16.85	13.20	29,568	20.79	15.75	35,280	24.81
10.75	24,080	16.93	13.25	29,680	20.87	15.80	35,392	24.88
10.80	24,192	17.01	13.30	29,792	20.95	15.85	35,504	24.96
10.85	24,304	17.09	13.35	29,904	21.03	15.90	35,616	25.04
10.90	24,416	17.17	13.40	30,016	21.10	15.95	35,728	25.12
10.95	24,528	17.25	13.45	30,128	21.18			
			13.50	30,240	21.26	16.00	35,840	25.20
11.00	24,640	17.32	13.55	30,352	21.34	16.05	35,952	25.28
11.05	24,752	17.40	13.60	30,464	21.42	16.10	36,064	25.36
11.10	24,864	17.48	13.65	30,576	21.50	16.15	36,176	25.44
11.15	24,976	17.56	13.70	30,688	21.58	16.20	36,288	25.51
11.20	25,088	17.64	13.75	30,800	21.66	16.25	36,400	25.59
11.25	25,200	17.72	13.80	30,912	21.73	16.30	36,512	25.67
11.30	25,312	17.80	13.85	31,024	21.81	16.35	36,624	25.75
11.35	25,424	17.88	13.90	31,136	21.89	16.40	36,736	25.83
11.40	25,536	17.95	13.95	31,248	21.97	16.45	36,848	25.91
11.45	25,648	18.03				16.50	36,960	25.99
11.50	25,760	18.11	14.00	31,360	22.05	16.55	37,072	26.07
11.55	25,872	18.19	14.05	31,472	22.13	16.60	37,184	26.14
11.60	25,984	18.27	14.10	31,584	22.21	16.65	37,296	26.22
11.65	26,096	18.35	14.15	31,696	22.29	16.70	37,408	26.30
11.70	26,208	18.43	14.20	31,808	22.36	16.75	37,520	26.38
11.75	26,320	18.51	14.25	31,920	22.44	16.80	37,632	26.46
11.80	26,432	18.58	14.30	32,032	22.52	16.85	37,744	26.54
11.85	26,544	18.66	14.35	32,144	22.60	16.90	37,856	26.62
11.90	26,656	18.74	14.40	32,256	22.68	16.95	37,968	26.70
11.95	26,768	18.82	14.45	32,368	22.76			
			14.50	32,480	22.84	17.00	38,080	26.77
12.00	26,880	18.90	14.55	32,592	22.92	17.05	38,192	26.85
12.05	26,992	18.98	14.60	32,704	22.99	17.10	38,304	26.93
12.10	27,104	19.06	14.65	32,816	23.07	17.15	38,416	27.01
12.15	27,216	19.14	14.70	32,928	23.15	17.20	38,528	27.09
12.20	27,328	19.21	14.75	33,040	23.23	17.25	38,640	27.17
12.25	27,440	19.29	14.80	33,152	23.31	17.30	38,752	27.25
12.30	27,552	19.37	14.85	33,264	23.39	17.35	38,864	27.33
12.35	27,664	19.45	14.90	33,376	23.47	17.40	38,976	27.40
12.40	27,776	19.53	14.95	33,488	23.55	17.45	39,088	27.48
12.45	27,888	19.61				17.50	39,200	27.56
12.50	28,000	19.69	15.00	33,600	23.62	17.55	39,312	27.64





## APPENDIX IV.

## RAPID DETERMINATION OF PHOSPHORUS AND MANGANESE.

THE following rapid methods of determining Phosphorus and Manganese may be found useful. The method for Phosphorus only gives comparative and very approximate results, but is useful for determining whether this constituent is above or below a certain limit in the bath of a basic Siemens furnace previous to tapping. The Manganese method gives excellent results, even as compared with the gravometric method.

## PHOSPHORUS.—Solutions required—

- No. 1, 400 grms. of Ammonium Nitrate + 500 c.c. Nitric Acid made up to 1,000 c.c.  
 No. 2, 50 grms. of Ammonium Molybdate + 100 grms. Ammonium Nitrate made up to 1,000 c.c.

2 gm. of the steel is dissolved in 4 c.c. of No. 1 solution in a 6-inch test tube 1 inch in diameter, and is warmed; when dissolved, 4 c.c. of No. 2 solution are added, and the liquid heated to just the boiling point, diluted with hot water to a mark to fill tube one-third full, well agitated, and compared for turbidity with two standard steels, treated under identical conditions. Assuming it is necessary that the steel should contain less than .08 per cent. Phosphorus, but not less than .05 per cent., two standards of these percentages, respectively, are used. The comparison can be made in a few minutes, and enables the sample passer to say if the Phosphorus is well under .08 per cent., and if the bath is ready to be tapped.

## MANGANESE, WALTER'S METHOD.—Solutions—

- Nitric Acid, specific gravity 1.2.  
 Nitrate of Silver, 1.33 grms. in 1,000 c.c. of water.  
 Ammonium Persulphate, 10 grms. dissolved in 30 c.c. of cold water *immediately before use.*

Dissolve .1 gm. of steel in 5 c.c. of the acid, and heat in a water-bath until all nitrous fumes are expelled. Add  $7\frac{1}{2}$  c.c. of Nitrate of Silver solution and 3 c.c. of Ammonium Persulphate solution, well mix by pouring solution to and from a clean test tube, place in water-bath (not allowing water to boil), and warm for about two minutes after oxidation commences. Cool in cold water, and compare with standard steels containing known percentages of Manganese treated under identical conditions. It is absolutely necessary that fresh Ammonium Persulphate solution should be prepared every time.

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